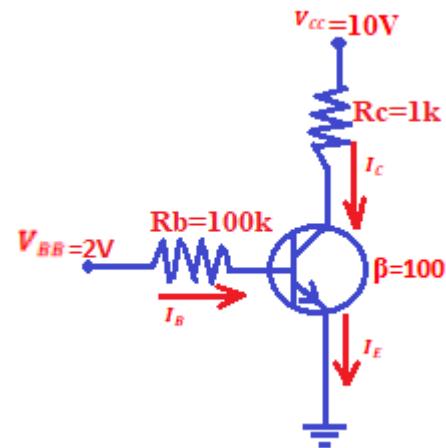
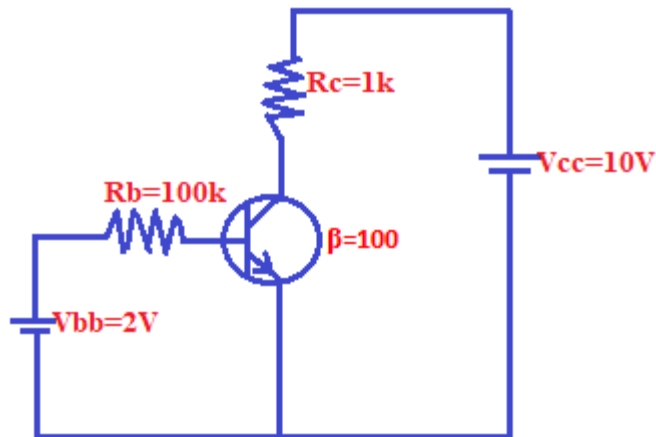


BIPOLAR JUNCTION TRANSISTOR II

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$V_{BE} = 0.7 \text{ V}$, as emitter is grounded $V_B = 0.7 \text{ V}$

$$V_{BB} = I_B R_B + V_{BE}$$

$$2 \text{ V} = I_B \cdot 100\text{k} + 0.7 \text{ V}$$

$$I_B = \frac{2 - 0.7}{100} \times 10^{-3} \text{ amp}$$

$$I_B = 13 \mu\text{A}$$

$$I_C = \beta I_B = 100 \times 13 \mu\text{A} = 1.3 \text{ mA}$$

$$V_{CC} = I_C R_C + V_{CE} \Rightarrow V_{CE} = V_{CC} - I_C R_C = 10 - 1.3 = 8.7 \text{ V}$$

$$V_{BC} = V_B - V_C = 0.7 - 8.7 = -8 \text{ V}$$

Thus the collector-base junction is reverse biased.

Three primary currents which flow across the forward biased emitter junction and reverse biased collector junction are I_E , I_B , and I_C

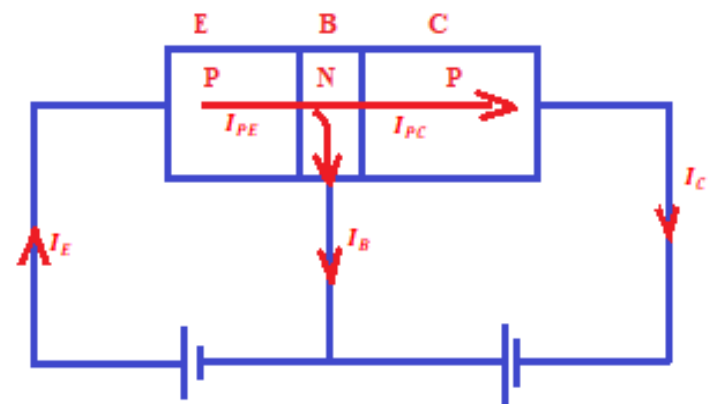
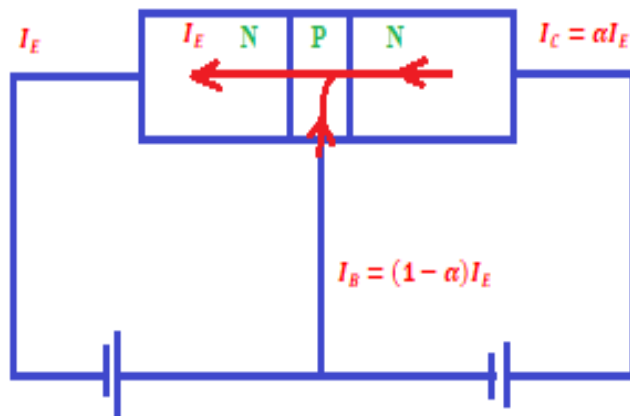
$$I_E = I_B + I_C$$

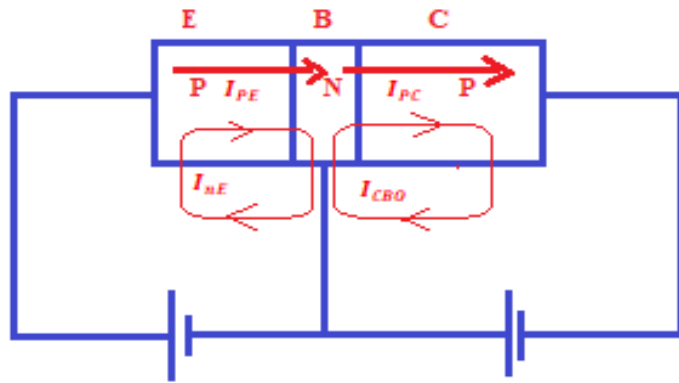
Also $I_C = \alpha I_E$

$$\begin{aligned} I_B &= I_E - I_C \\ &= (1 - \alpha)I_E \\ &= (1 - .98)I_E \\ &= 0.02I_E \end{aligned}$$

So considering the current due to the majority carriers, the emitter current split into two parts

- (i) $(1 - \alpha)I_E$ which becomes base current I_B in the external circuit, and
- (ii) αI_E which becomes collector current I_C in the external circuit.





In PNP transistor collector-base junction is reverse biased for majority charged carriers but it is forward biased for thermally generated minority carriers.

The current flow in the same direction of I_C due to the minority carriers, called leakage current and denoted by I_{CBO} .

This current flows even when emitter is disconnected from the dc supply source

This current is extremely temperature dependent

Similarly I_{nE} flows in the emitter base junction

The emitter current I_E consists of the hole current I_{pE} and electron current I_{nE}

$$\text{i. e. } I_E = I_{pE} + I_{nE}$$

The collector current I_C consists of I_{pC} and the temperature dependent current I_{CBO} due to the minority carriers

$$\begin{aligned} \text{i. e. } I_C &= I_{pC} + I_{CBO} \\ &= \alpha I_E + I_{CBO} \end{aligned}$$

$$\text{Thus } \alpha = \frac{I_C - I_{CBO}}{I_E}$$

I_B depends on $I_{pE}, I_{pC}, I_{nE}, I_{CBO}$

Emitter efficiency, $\gamma = \frac{\text{current of injected carriers from the emitter}}{\text{total current}}$

$$= \frac{I_{pE}}{I_{pE} + I_{nE}}$$

$$= \frac{I_{pE}}{I_E}$$

We may say $I_{pE} \gg I_{nE}$

$$\gamma = \frac{1}{\left(1 + \frac{I_{nE}}{I_{pE}}\right)} = 1 - \frac{I_{nE}}{I_{pE}}$$

Transport factor β^* , also known as base transport factor

$$\beta^* = \frac{\text{injected carrier current reaching collector junction}}{\text{injected carrier current at emitter junction}}$$

$$= \frac{I_{pC}}{I_{pE}}$$

The collector efficiency, δ is the ratio of the current crossing the collector junction to the current arriving at the base side of the junction

We know

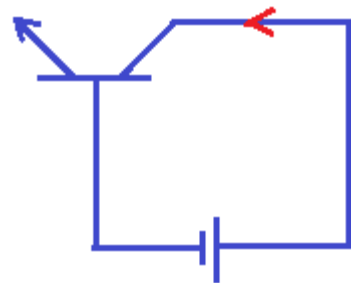
$$\alpha = \frac{I_C - I_{CBO}}{I_E}$$

$$= \frac{I_{pC}}{I_E}$$

$$= \frac{I_{pC}}{I_{pE}} \times \frac{I_{pE}}{I_E} = \beta^* \cdot \gamma$$

LEAKAGE CURRENTS

1. COLLECTOR TO BASE LEAKAGE CURRENT (I_{CBO})



The collector current I_C consists of

(i) The part of emitter current I_E which reaches the collector, and

(ii) The collector-base leakage current I_{CBO} or I_{CO}

Thus the part of I_E which reaches collector is equal to $I_C - I_{CBO}$

$$\alpha = \frac{I_C - I_{CBO}}{I_E}$$

$$I_C = \alpha I_E + I_{CBO}$$

We know

$$I_E = I_C + I_B$$

Therefore

$$I_C = \alpha(I_C + I_B) + I_{CBO}$$

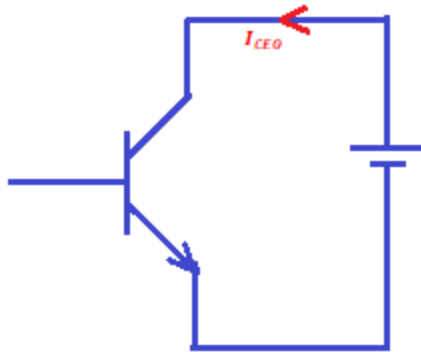
$$I_C(1 - \alpha) = \alpha I_B + I_{CBO}$$

$$I_C = \frac{\alpha}{1 - \alpha} I_B + \frac{1}{1 - \alpha} I_{CBO}$$

$$I_C = \beta I_B + (\beta + 1) I_{CBO}$$

2. COLLECTOR TO EMITTER LEAKAGE CURRENT (I_{CEO})

When base is open circuited and collector is reverse biased with respect to emitter,



a small current I_{CEO} flows from collector to emitter.

The collector current consists of

(i) The part of the emitter current I_E which reaches the collector, and

(ii) The collector emitter leakage current I_{CEO}

The part of I_E , which reaches collector is $I_C - I_{CEO}$

Thus when leakage current is taken into consideration the equation for β can be written as

$$\beta = \frac{I_C - I_{CEO}}{I_B}$$

$$I_C = \beta I_B + I_{CEO}$$

$$I_C = \beta I_B + (\beta + 1)I_{CBO}$$

Also we have

Equating

$$I_{CEO} = (\beta + 1)I_{CBO}$$

We know the relation between α and β as

$$\beta = \frac{\alpha}{1 - \alpha}$$

Let us take some values of α and calculate corresponding value of β

α	β
0.9	9
0.95	19
0.99	99
0.995	199
0.999	999

Thus a change in α by 1% introduces a large change in β
The leakage current I_{CBO} of the reverse biased collector base junction changes greatly with temperature

An increase in temperature increases the value of I_{CBO}
since $I_C = \beta I_B + (\beta + 1)I_{CBO}$

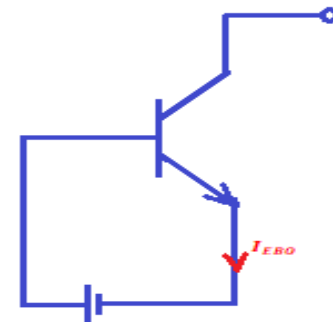
An increase in I_{CBO} increases I_C

The increase of I_C increases the power dissipation at the collector junction and thereby increases the junction temperature.

The increase of temperature further increases I_{CBO}

3. EMITTER TO BASE LEAKAGE CURRENT (I_{EBO})

When the collector is open circuited and the emitter base junction is reverse biased, a small emitter current flows through the emitter base junction.



CHARACTERISTICS OF TRANSISTOR

The method of connection of a transistor into a circuit largely affects input and output impedances, and characteristics of the transistor will vary according to the method of connection

The three methods of connections are

- (i) Common base
- (ii) Common emitter, and
- (iii) Common collector

